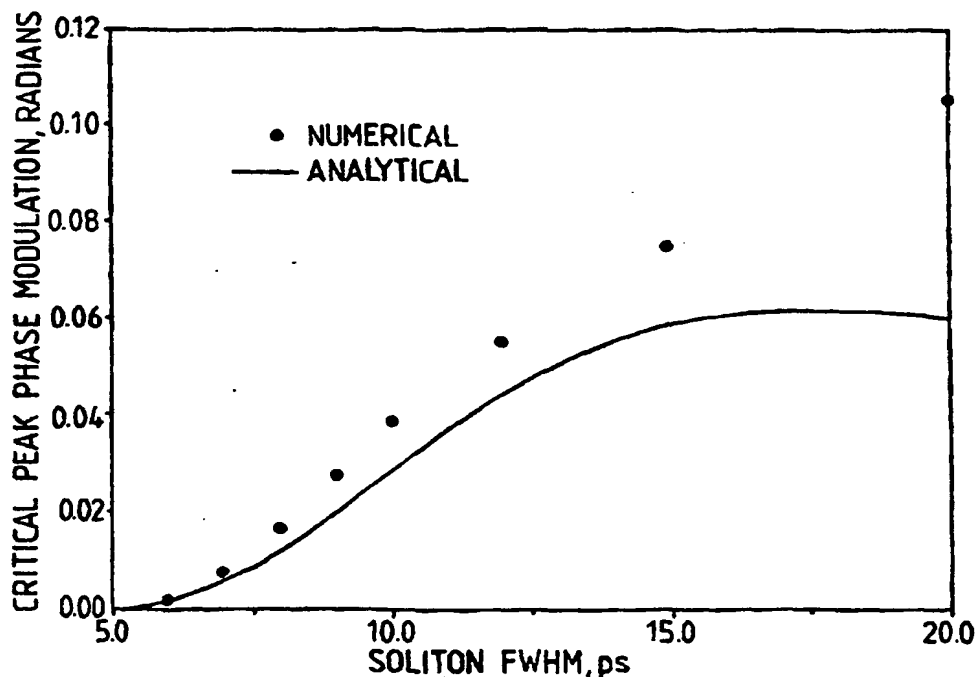




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(54) Title: OPTICAL SYSTEM



(57) Abstract

The invention relates to the control of soliton-soliton interaction through the application of a positive phase shift. For each soliton width there is a critical phase modulation level above which soliton-soliton interaction can be virtually eliminated. This enables the spacing between adjacent solitons to be reduced, increasing the system bandwidth even for long transmission distances. The invention finds application in submarine and other long haul systems.

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OPTICAL SYSTEM

The present invention relates to optical systems and in particular optical systems within which optical solitons
5 are propagated.

The word soliton was first coined by Zabusky and Kruskal to describe the particle-like behaviour of the solitary wave solutions of the numerically treated Korteweg-deVries equation. Now, more than 100 different non-linear
10 partial differential equations exhibit soliton-like solutions. Optical solitons belong to the class of envelope solitons and can be described by the non-linear Schrodinger (NLS) equation.

Hasegawa and Tappert in 1973 were the first to show
15 theoretically that, in an optical fibre, solitary waves were readily generated and that the NLS equation description of the combined effects of dispersion and the non-linearity self-phase modulation, gave rise to envelope solitons. It was not until seven years later, in 1980 that Mollenauer and
20 co-workers first described the experimental realization of the optical soliton, the delay primarily being due to the time required for technology to permit the development of low loss single-mode fibres. Since 1980 there has been tremendous research effort in the field of optical solitons,
25 the research being driven by the promise of massively increased bit rates, through the application of ultra short soliton pulses in long-distance optical communication networks. In addition, solitons are attractive for use in ultra fast optical switching and processing, primarily based
30 on interferometric techniques.

Unfortunately, additional non-linearities which had not been considered originally have put limits on potential systems for long distance optical communication. Nevertheless, it is likely that optical soliton systems for
35 long distance optical communication, for example transatlantic systems, will be installed within five years or so. Nevertheless, the raising of the limits on transmission

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distance remains a focus of much research. Similarly, the related problem of stability in switching and storage systems which use optical solitons is a major focus of much current research.

5 One of the main constraints on the design of optical fibre soliton communication systems is the interaction force which exists between adjacent pulses in the bit stream, see J P Gordon, Optics Letters, 8, (1983), page 596; K J Blow, N J Doran, Electronics Letters, 19, (1983), 429-430; P L Chu, 10 C Desem, Electronics Letters, 19, (1983), 956-957. It has been shown that bandwidth filtering or temporal modulation are effective means of combatting the other source of timing errors in such systems, namely Gordon-Haus jitter. However, spectral filtering has relatively little effect on the 15 interaction forces when proper account is made of the evolved pulse parameters, see M Nakazawa, H Kubota, Electronics Letters, 20, 28, (1992), 958-960. Wabnitz has shown, Optics Letters, 18, (1993), 601-603, in the context of a ring cavity, that the interactions may be controlled by the 20 injection of a low amplitude cw wave; however this technique is less suited for use in transmission systems. Recently Francois Georges examined, Optics Letters, 18, (1993) 583-585, the use of a combined phase and amplitude modulation cycle to suppress the interactions. In that work 25 neighbouring pulses were placed at opposite extrema of the phase modulation component, thus breaking the coherence between them. The modulation function in question was however, somewhat unphysical. Additionally the present inventors have shown elsewhere that one extremum of a phase 30 modulator's cycle enhances the Gordon-Haus jitter, see N J Smith, K J Blow, D J Firth, K Smith, Optics Communications, Vol. 102, 324-238, 1993.

In our above-mentioned paper, we disclose that a positive phase modulation may be used to reduce Gordon-Haus 35 jitter. However, as indicated above in relation to bandwidth filtering and temporal modulation, while techniques have been devised for controlling Gordon-Haus jitter, the control of

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soliton-soliton interactions has proved to be much more difficult.

Surprisingly, the inventors have discovered that it is possible to control soliton-soliton interaction by applying
5 phase modulation in an appropriate fashion. In this way it is possible to increase the interaction lengths dramatically.

According to the present invention there is provided a method of propagating optical solitons in which a positive phase modulation is imposed on solitons after they have
10 propagated at least 30 kilometres along an optical fibre transmission path, the amount of phase modulation imposed being sufficient to maintain the temporal separation between adjacent solitons so that significant soliton-soliton interactions are avoided.

15 In a second aspect the present invention provides an optical transmission system in which phase modulation is applied to increase the interaction length for optical solitons propagating in the system.

According to a further aspect the present invention
20 provides a submarine communication system comprising an optical fibre communications path at least 1,000 miles in length which includes a plurality of phase modulators spaced along the fibre communication path, which phase modulators impose a phase modulation sufficient to prevent significant
25 interaction between solitons propagated along the fibre. According to a further embodiment the present invention provides an optical fibre ring or loop within which at least one optical soliton circulates, the loop including at least one phase modulator which imposes a phase modulation
30 sufficient to ensure the stability of the system.

In a further aspect the present invention provides an optical communications system comprising a source of optical solitons coupled to an optical fibre transmission path, the optical fibre transmission path including a phase modulator,
35 the phase modulator being modulated in use at a frequency such that adjacent solitons pass through consecutive upchirped peaks of the modulation cycle, the modulator

inducing corrections to a soliton frequency in response to changes in the soliton's temporal position.

According to a further aspect the present invention provides a method or apparatus in which solitons are exposed
5 to phase modulation above the critical level, whereby soliton-soliton interactions are substantially reduced.

Embodiments of the invention will now be described with reference to the accompanying drawings in which:

Figure 1a is a plot of soliton frequency against
10 soliton position in the form of a phase space portrait;

Figure 1b is a similar plot showing the phase space portrait when no equilibrium points occur;

Figure 2 is a plot of the observed collision lengths as a function of applied modulator strength; and

15 Figure 3 is a plot of critical peak phase modulation against soliton width;

Figure 4 is a plot of collision lengths of 6ps solitons separated by 40ps as a function of imposed positive phase modulation; and

20 Figure 5 is a similar plot for 10ps solitons.

An isolated pair of in phase solitons,

$$u = A \operatorname{sech}((t - T_0)/\tau) + A \operatorname{sech}((t + T_0)/\tau) \dots (1)$$

undergo a bound oscillation, the first collision occurring at
25 a distance $z_c - (z_0/2) \exp(T_0/\tau)$, where z_0 is the soliton period. There are two possible approaches when solving the initial value problem to the non-linear Schrodinger equation (NLSE) posed by equation 1. The full second order soliton solution may be constructed, for example using the (non-
30 degenerate) eigenvalues of the inverse scattering transform [1, 7, 8]. Alternatively, the dynamics may be regarded as composed of two identical individual solitons, each acting as a perturbation on the other [10]. The latter scheme readily admits the incorporation of extra effects, such as external
35 modulation, and is employed here. The method is valid only when the two pulses do not strongly overlap; thus it is

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useful for small motions around initially separate positions and the stability thereof, which is the main concern here. Our scheme is to place phase modulators periodically along the optical fibre, and to set the modulation frequency such

5 that adjacent solitons pass through consecutive upchirped peaks of the modulator cycle. (The use of truly consecutive upchirped peaks is of course not essential. One could run the modulator at twice this rate, or some higher multiple of it, so that some peaks do not 'see' solitons. This would

10 require a modulator capable of running at the higher rate, and there would appear to be little to gain from this approach.) The modulator induces corrections to a soliton's frequency, and hence speed, in response to changes in its temporal position caused by the interaction forces. If these

15 affects combine to produce a stable equilibrium position, collisions between solitons will be suppressed. If no equilibrium point exists, then the global behaviour (ie collision) will not be averted. Because the interaction forces decrease exponentially with separation, only nearest

20 neighbour effects need to be considered. An isolated pair is the worst case scenario, and so our model applies to both random bit patterned and uniform sequences of solitons. Using the perturbational methods [10], ordinary differential equations may be derived for the parameters of each soliton,

25 $u_i = (A/\tau) \operatorname{sech}((t-T_i)/\tau) e^{i\omega_i t}$, for $i = 1, 2$:

$$\frac{d\omega_i}{dz} = (-1)^i \frac{4\beta}{T^3} e^{-z/T} - 2\alpha_m (T_i - T_{i0}) \quad (2)$$

30

$$\frac{dT_i}{dz} = \beta \omega_i \quad (3)$$

Here $r = T_1 - T_2$ is the pulse separation, and T_{i_0} the peaks in the modulation cycle. For modulators with spacing l and transfer function $u_{out} = u_{in} \exp(i\Phi \cos(\omega_m t))$, $\alpha_m = \Phi \omega_m^2 / 2l$. In the light of our previous work, both solitons are initially placed at upchirped peaks of the modulator cycle. It has been assumed that the modulators are spaced sufficiently closely to average their action over the length of the fibre. As the motion is symmetric, attention will be focused on the $i=1$ soliton and the subscripts dropped. Note that now $r=2T$.

Introducing $\Delta T = T - T_0$,

$$\frac{d\omega}{dz} = -\frac{4\beta}{\tau 3} e^{-2(T_0 + \Delta T)/\tau} - 2\alpha_m \Delta T \quad (4)$$

$$\frac{d\Delta T}{dz} = \beta \omega \quad (5)$$

Examination reveals that equation 4 may have either 0 or 2 fixed points, depending upon the strength of α_m . The consequence of the point's existence is that a harmonic potential well is present, around which the soliton's frequency and position perform a closed orbit, as shown by the phase space portrait in Figure 1a. Provided the initial point lies inside the separatrix the two pulses each remain trapped in their separate potentials, ie modulator cycle peaks. When no equilibrium points occur the phase space is as illustrated in Figure 1b, and the soliton's interaction is essentially unimpeded. In the language of non-linear dynamics, the two cases are separated by a subtle-node bifurcation; the singularity at the critical point being terms cuspidal.

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These predictions are confirmed by the results of a numerical integration of the full NLSE completely with periodically spaced phase modulators. The observed collision lengths are plotted in Figure 2 as a function of applied modulator strength. The parameters used are $\tau=6.25\text{ps}$ approximately equal to 10ps FWHM, $T_0=20\text{ps}$, $\beta=1.25\text{ps}^2$ per kilometre, $l_m=30\text{km}$ and $\omega_m=2\pi \cdot 25\text{GHz}$. Below the critical point, the phase modulator only changes the collisions length by factors of less than 3. Above the critical point the collision lengths rise very rapidly indeed with increased modulation. The phase space diagram suggests that in this region the collision lengths should be infinite; however examination of the full field profile show that over long distances the pulse pairs develop some asymmetry, followed by an interaction. This is inconsistent with the perturbation theory, but is to be expected due to the non-degenerate IST eigenvalues and the imaginary (ie reactive) coefficient of the modulator term.

It remains to calculate the bifurcation point. Notice that at the critical value of α_m , the two functions on the right hand side of equation 4 intersect tangentially. Thus the derivative with respect to δT is then also 0:

$$0 = \frac{4\beta}{\tau^3} \frac{2}{\tau} e^{-2T_0/\tau} e^{-2\Delta T/\tau} - 2\alpha_m \quad (6)$$

Solving these two conditions as simultaneous equations gives,

$$\Delta T = -\frac{\tau}{2} \quad (7)$$

$$\alpha_m = \frac{4\beta}{\tau^4} \exp\left(1 - \frac{2T_0}{\tau}\right) \quad (8)$$

5 The value of Φ implied by equation 8 is plotted in Figure 3 as a function of pulse width with $T_0=20\text{ps}$, $l=30\text{km}$. Also shown are the numerically observed bifurcation points from our integrations of the NLSE. It can be seen that there is good agreement for small pulse widths (large interpulse spacings),
 10 which gradually diverges as the overlap between pulses becomes stronger. Some of the discrepancy will be accounted for by the fact that the separatrix must be sufficiently large to include the initial point before its presence is detected by the numerical simulation.

15 Thus it is clear that application of sufficient phase modulation will suppress soliton-soliton interactions. The analytical calculation of the critical value shows reasonable agreement with the numerically observed values. It is predicted that future trans-oceanic systems will have bit
 20 rates of the order of 10 to 20gbit/s over lengths of 6,000 to 10,00 km.

$$L_{coll} = \int_0^{-T_0} \left(\frac{4\beta^2}{\tau^2} e^{-\frac{2T_0}{\tau}} \left(e^{-\frac{2\Delta T}{\tau}} - 1 \right) - 2\alpha_{m2}\beta\Delta T \right)^{\frac{1}{2}} d\Delta T$$

25

where the pulse separation is $2T_0$,

β is the fibre dispersion,

τ is the pulse 'sech' width;

30 and α_{m2} is the phase modulator strength, ($\alpha_{m2} = \phi \omega_m / 2L_m$, where L_m is the modulator spacing, ϕ is the peak phase excursion and ω_m the angular drive frequency of the modulator).

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The collision distances of soliton pairs in dispersion shifted fibre (ie with D-1ps/nm/km) are, without phase modulation, as follows:

	<u>Soliton Period</u> <u>Z_0 Kilometres</u>	<u>Pulse Full Width</u> <u>$\frac{1}{2}$ Maximum,</u> <u>Picosecond</u>	<u>Bit Rate</u> <u>gbit/s</u>	<u>Collision</u> <u>Distance</u> <u>Kilometres</u>
5				
10	40	10	5 10 20	10^9 130,000 1,600
15	160	20	5 10 20	5×10^5 6,000 700
20	1,000	50	5 10 20	17,000 3,000 1,000

In a real system a safe margin would be to limit the system length to half the above distances. Moving to shorter pulse widths is not a universal panacea; it incurs other system penalties, notably Gordon-Haus jitter and "average soliton model" limits. Currently, a soliton pulse width (FWHM) of 20ps is regarded as about optimum.

Clearly, an important benefit of controlling soliton-soliton interaction according to the invention is that the spacing between solitons can be reduced, thereby increasing the system bandwidth, even for long haul systems.

The phase modulators should be able to suppress interactions for any modulator spacing which is small compared to the interaction length, say a factor of 2 to 3. Nevertheless, the validity of the above quantitative predictions as to the required phase modulator strength are probably limited, for the numerical examples presented, to modulator spacings of up to about 50km. That is, with modulator spacings of more than 50km slightly more phase modulation may need to be imposed that is suggested in the above quantitative predictions.

While one could use electrooptic or other electrically driven phase modulators, it is also possible to impose sufficient modulation using some all-optical system. Of course, with the electrically driven modulators some means
5 needs to be provided to synchronise the modulation with the incoming pulse strength - that is some form of clock extraction is required to provide a suitably synchronised electrical signal. Again, recently developed all-optical clock extraction systems could be used to provide an
10 optically driven phase modulator.

A suitable system for all-optical clock recovery is described in the Applicant's co-pending International patent application, application number GB93/00863 (Agent's ref: A24455) filed on 26 April 1993, published as WO93/22855, and
15 which is herein incorporated by this reference. The phase modulation required to be imposed in accordance with the present invention can of course be cross phase modulation.

It should also be noted that the present invention is applicable not only to solitons at a single wavelength but
20 also to solitons of different wavelengths propagating down a common fibre.

In long haul soliton transmission systems, such as transoceanic submarine systems, it is likely that repeaters will be provided at approximately 30 to 50 kilometre
25 intervals and will contain optical amplifiers to keep the signal level sufficiently high. Typically, such amplifiers will be fibre-based devices, e.g. rare-earth doped fibre amplifiers (erbium fibre amplifiers are suitable for the 1.5 μ m window, praseodymium for the 1.3 μ m window). Clearly in
30 such systems it would make sense to incorporate within such repeaters the phase modulators required by the present invention. Of course where the requisite phase modulation can be provided by cross phase modulation within an optical fibre it is possible that part of the transmission fibre
35 could provide the medium within which the phase modulation occurs and as such the relevant fibre portion might be within or outside a repeater.

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Typically the soliton wavelength would be in the 1.5 micron (eg 1.55) transmission window of silica fibre - assuming the use of silica fibre as the transmission medium. A suitable soliton source for such systems is described in
5 our co-pending international patent application WO 91/18593 (Agent's ref A24298) and the corresponding US patent application 946464 (filed 18.11.92) which are herein incorporated by this reference.

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CLAIMS

1. An optical communications system comprising a source of optical solitons coupled to an optical fibre transmission path, the optical fibre transmission path including at least one phase modulator which is modulated at a frequency such that adjacent solitons pass through upchirped peaks of the modulation cycle, the modulator inducing corrections to a soliton's frequency in response to changes in the soliton's temporal position caused by interaction forces.
2. An optical communications system as claimed in claim 1, wherein the solitons pass through consecutive upchirped peaks.
3. An optical communications system as claimed in claim 1 or claim 2, wherein multiple phase modulators are provided along the transmission path, the adjacent phase modulators being substantially equally spaced from each other.
4. An optical communications system as claimed in claim 3, wherein the separation between adjacent phase modulators is between 30 and 60km.
5. An optical communications system as claimed in any one of claims 1 to 4 wherein the or each phase modulator is an electro-optic device.
6. An optical communications system as claimed in any one of claims 1 to 4, wherein the or each phase modulator is an all-optical device.
7. An optical communications system as claimed in any one of the preceding claims, wherein the soliton width (FWHM) is not more than 10ps and the or each phase modulator applies a positive phase modulation of at least 0.04 radians.

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8. An optical communications system as claimed in any one of claims 1 to 6, wherein the soliton width (FWHM) is about 15ps and the or each phase modulator applies a positive phase modulation of at least 0.065 radians.
- 5 9. An optical communications system as claimed in any one of claims 1 to 6, wherein the soliton width (FWHM) is about 20ps and the or each phase modulator applies a positive phase modulation of at least 0.10 radians.
- 10 10. An optical communications system as claimed in any one of the preceding claims, wherein the soliton width (FWHM) is no more than 25ps and the or each phase modulator applies a positive phase modulation of at least 0.10 radians.
- 15 11. An optical communications system as claimed in any one of the preceding claims, wherein adjacent solitons are separated by no more than 40ps.
- 20 12. An optical communications system as claimed in any one of the preceding claims wherein an optical amplifier is provided in the optical fibre transmission path at or near the site of the or each phase modulator.
- 25 13. An optical communications system as claimed in claim 12, wherein the or each amplifier has bandwidth filtering means.
- 30 14. A method of propagating solitons along an optical fibre communications route, in which a positive phase modulation is periodically imposed on the solitons as they traverse the route, the amount of phase modulation which is imposed being sufficient to maintain the temporal separation between adjacent solitons such that significant soliton-
35 soliton interactions are avoided.

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15. A method as claimed in claim 14, wherein the phase modulation is imposed at equally spaced locations along the communications route.
- 5 16. A method as claimed in claim 14 or claim 15, wherein the degree of phase modulation imposed at any location is selected in dependence upon the soliton width.
- 10 17. A method as claimed in any one of claims 14 to 16, wherein the soliton width (FWHM) is about 20ps and the degree of phase modulation imposed is at least 0.10 radians.
- 15 18. A method as claimed in any one of claims 14 to 17, wherein the phase modulation is imposed by electro-optic phase modulators.
19. A method as claimed in any one of claims 14 to 17, wherein the phase modulation is imposed through cross-phase modulation.

Fig.1.

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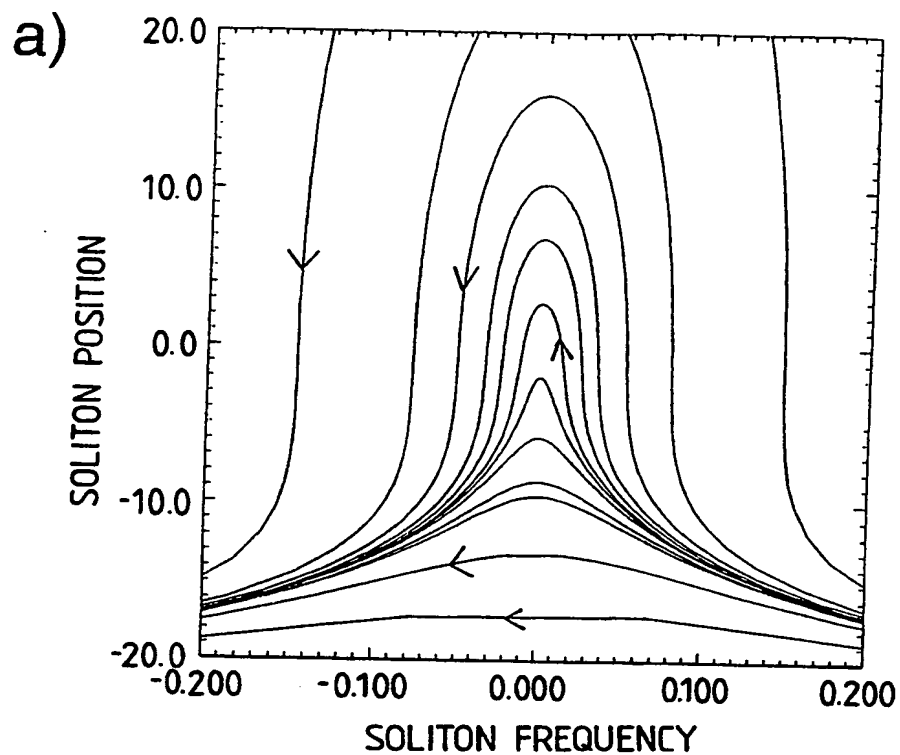
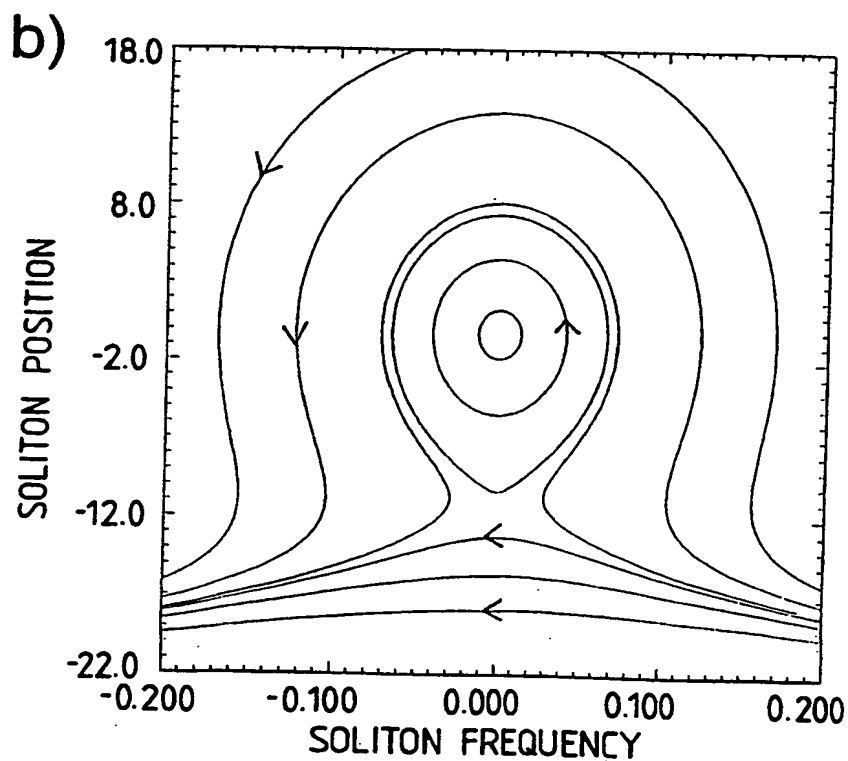


Fig.1.



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Fig.2.

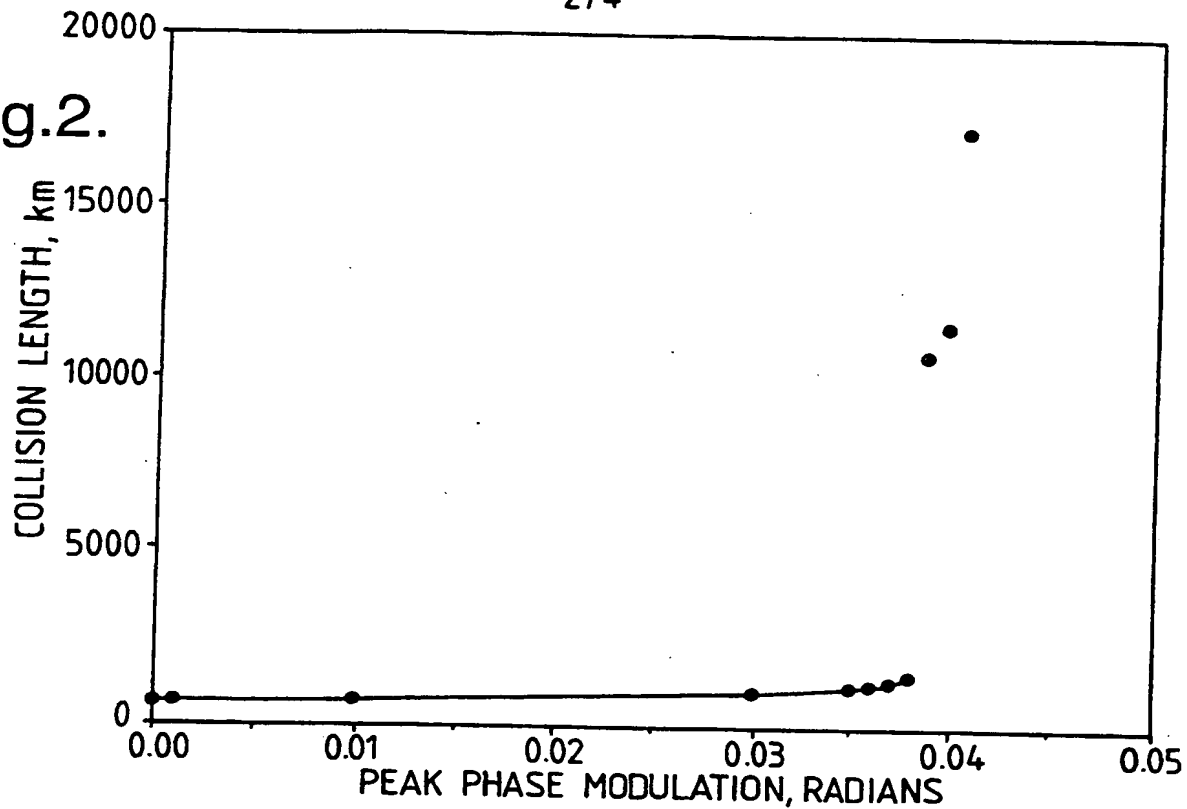
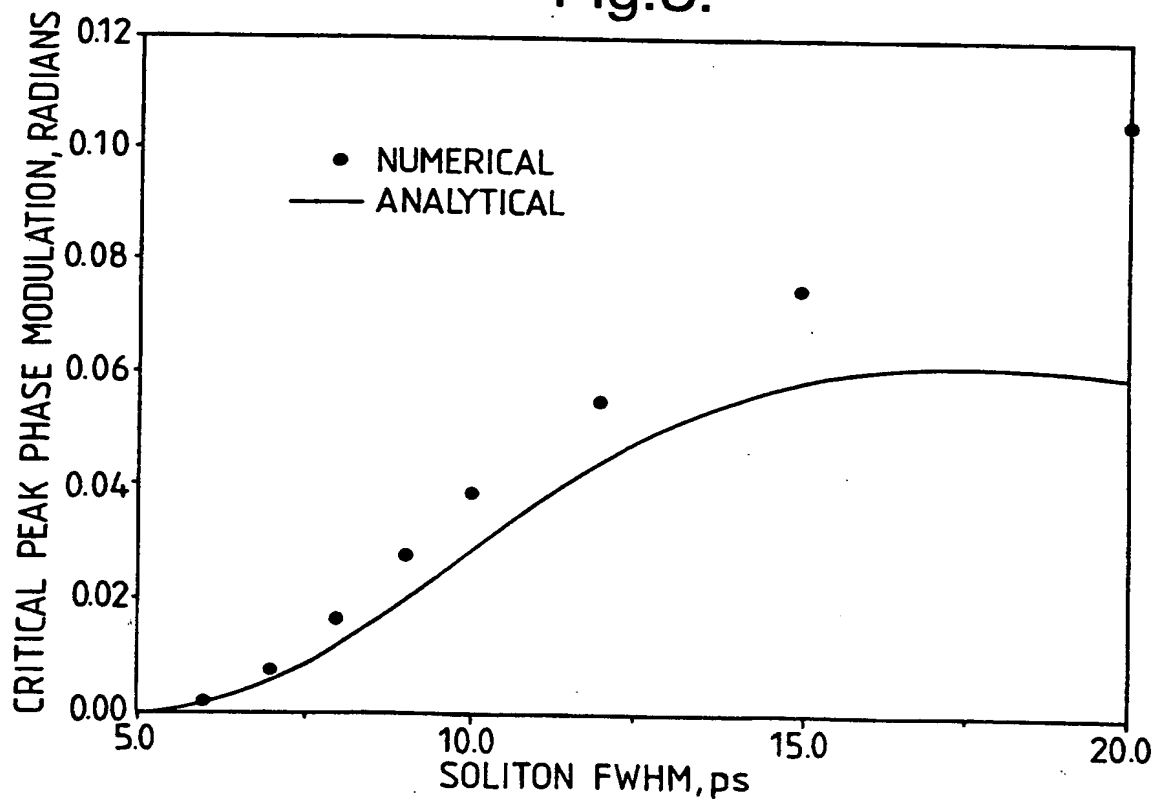


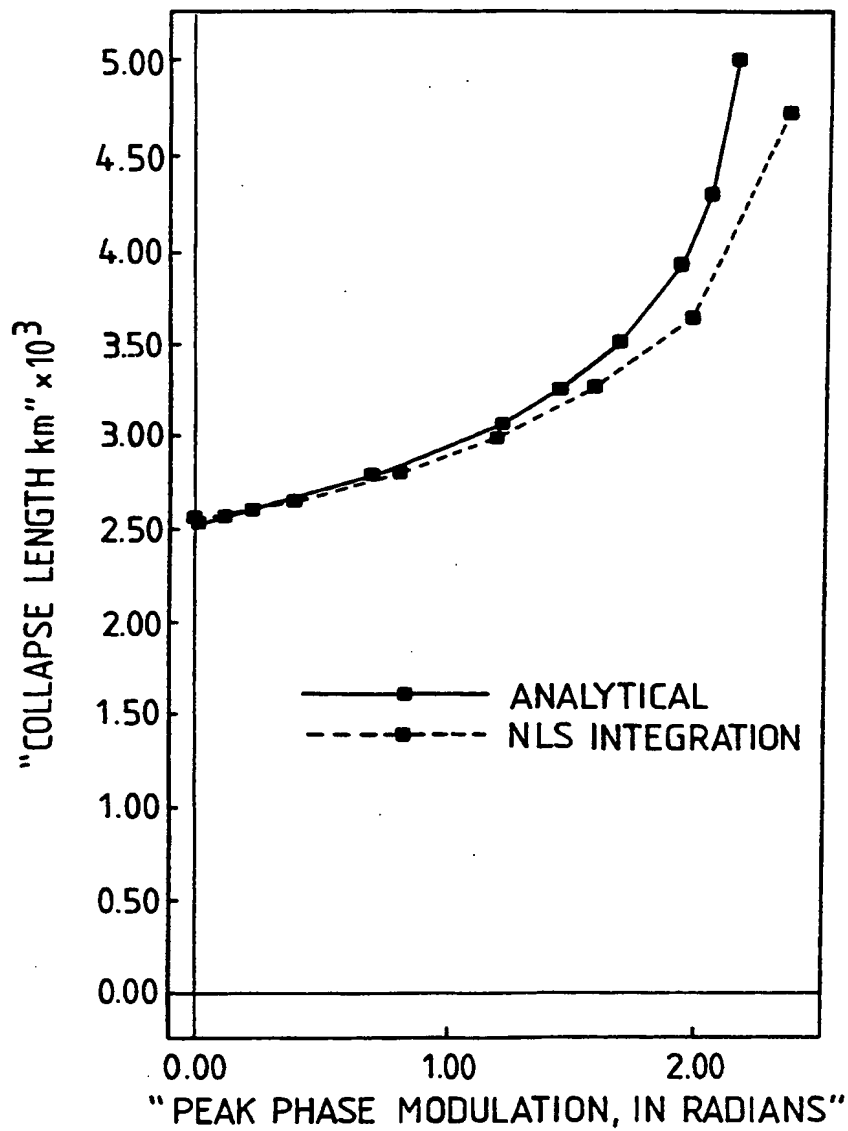
Fig.3.



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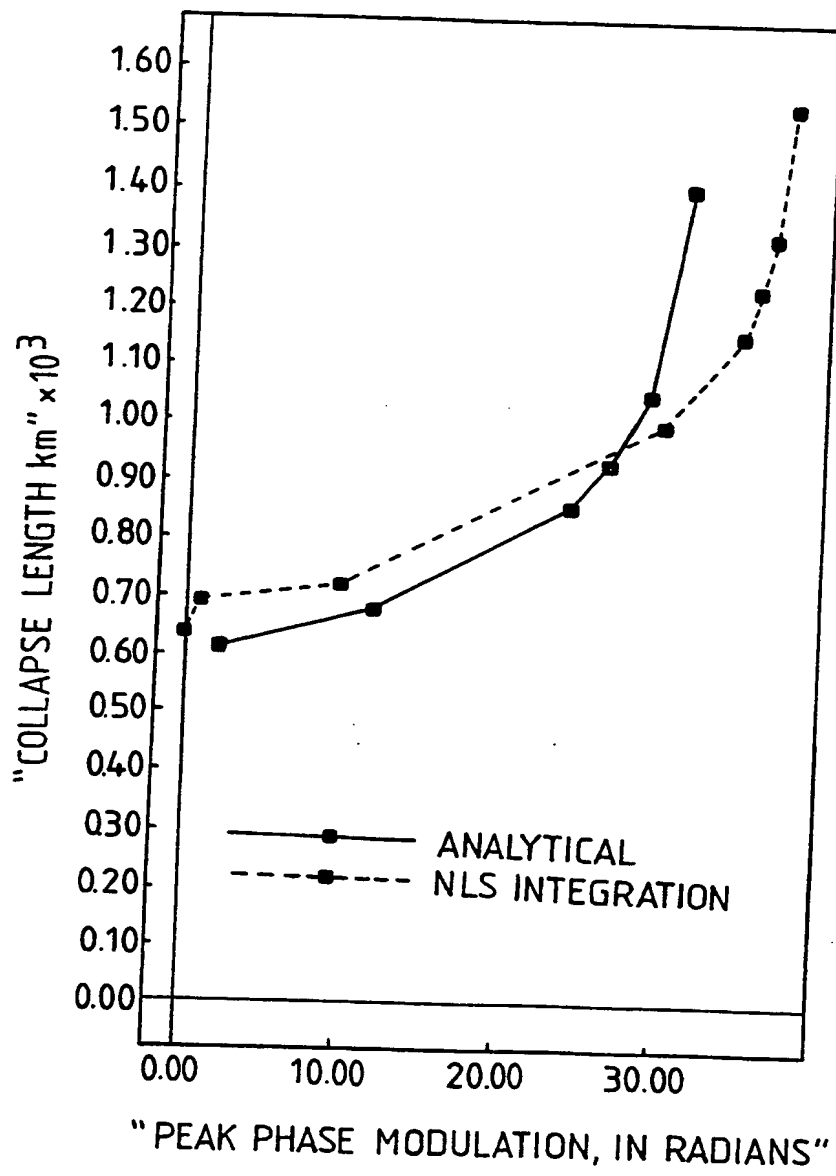
Fig.4.



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Fig.5.



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INTERNATIONAL SEARCH REPORT

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CT/GB 94/01750

A. CLASSIFICATION OF SUBJECT MATTER
 IPC 6 G02F1/35 H04B10/18

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
 IPC 6 G02F H04B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	OPTICS LETTERS., vol.18, no.8, 15 April 1993, NEW YORK US pages 583 - 585 P.L.FRANCOIS ET AL. 'Reduction of averaged soliton interaction forces by amplitude modulation' cited in the application see the whole document ---	1, 14
A	IEEE JOURNAL OF QUANTUM ELECTRONICS., vol.29, no.7, July 1993, NEW YORK US pages 2189 - 2197, XP000398739 H.KUBOTA ET AL. 'Soliton transmission control in time and frequency domains' see the whole document --- -/--	1, 14

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Date of the actual completion of the international search

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INTERNATIONAL SEARCH REPORT

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C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
P,X	OPTICS LETTERS., vol.19, no.1, 1 January 1994, NEW YORK US pages 16 - 18 N.J.SMITH ET AL. 'Suppression of soliton interactions by periodic phase modulation' see the whole document -----	1-19

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